

Material Measurement by Resonant Cavity Perturbation

Resonant cavities can be an extremely accurate method for measuring the EM properties of low loss materials.

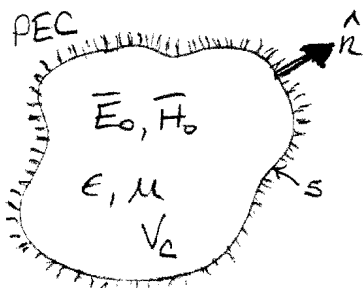
In one approach, the resonant frequencies and their associated Q's are measured with an empty cavity. Then a small sample is inserted into the cavity and the measurements are repeated for the <sup>downward</sup> shifted resonant frequencies and, typically, the reduced Q's. (There are other methods for resonant cavity measurements that don't involve small specimens, but these won't be considered here.)

No calibration is typically required. Just measure the changes in resonant freq and changes to Q.

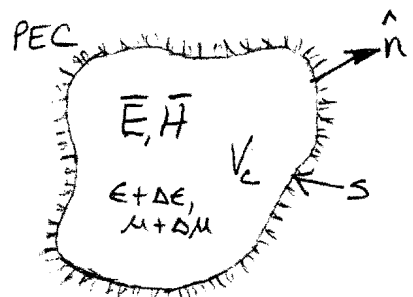
The difficult part is extracting the EM properties from these resonant cavities. A perturbation technique is often employed for this purpose. This technique assumes that the sample only slightly changes, or perturbs, the fields that exist without the sample present.

The equations used to perform this extraction are derived beginning w/ the Maxwell curl equations for two situations:

Unperturbed



Perturbed



The perturbed case - for now - will assume the material throughout the cavity has been changed.

# Exact Formula for Relative Change in Resonant Frequency

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✓ Harrington, THEF  
pp. 318-323

✓ Pozar, 3rd  
298-299

in a source free region

... Then,

$$-\nabla \times \bar{E}_0 = j\omega_0 \mu \bar{H}_0 \quad (1)$$

(1)

$$\nabla \times \bar{H}_0 = j\omega_0 \epsilon \bar{E}_0 \quad (2)$$

(2)

... While,

$$-\nabla \times \bar{E} = j\omega(\mu + \Delta\mu) \bar{H} \quad (3)$$

(3)

$$\nabla \times \bar{H} = j\omega(\epsilon + \Delta\epsilon) \bar{E} \quad (4)$$

(4)

... We've assumed the resonant frequencies of the cavity will change in the perturbed case, of course.

... We scalar multiply (4) by  $\bar{E}_0^*$  and the conjugate of (1) by  $\bar{H}$ :

$$\bar{E}_0^* \cdot \nabla \times \bar{H} = j\omega(\epsilon + \Delta\epsilon) \bar{E}_0^* \cdot \bar{E} \quad (5)$$

(5)

$$-\bar{H} \cdot \nabla \times \bar{E}_0^* = -j\omega_0 \mu^* \bar{H} \cdot \bar{H}_0^* = -j\omega_0 \mu \bar{H} \cdot \bar{H}_0^* \quad (6)$$

(6)

$\mu^* = \mu$

... In (6) we've assumed the material has no magnetic loss so that  $\mu^* = \mu$ . Adding (5) and (6),

$$\bar{E}_0^* \cdot \nabla \times \bar{H} - \bar{H} \cdot \nabla \times \bar{E}_0^* = j\omega(\epsilon + \Delta\epsilon) \bar{E}_0^* \cdot \bar{E} - j\omega_0 \mu \bar{H} \cdot \bar{H}_0^* \quad (7)$$

(7)

... Applying the vector i.d.  $\nabla \cdot (\bar{A} \times \bar{B}) = \bar{B} \cdot \nabla \times \bar{A} - \bar{A} \cdot \nabla \times \bar{B}$  to the LHS of (7),

$$\nabla \cdot (\bar{H} \times \bar{E}_0^*) = j\omega(\epsilon + \Delta\epsilon) \bar{E}_0^* \cdot \bar{E} - j\omega_0 \mu \bar{H} \cdot \bar{H}_0^* \quad (8)$$

(8)

... Likewise, we can perform analogous operations with (2) & (3) to find that

$$\nabla \cdot (\bar{H}_0^* \times \bar{E}) = j\omega(\mu + \Delta\mu) \bar{H}_0^* \cdot \bar{H} - j\omega_0 \epsilon \bar{E} \cdot \bar{E}_0^* \quad (9)$$

(9)

... We've assumed  $\epsilon^* = \epsilon$  (i.e., lossless dielectric material).

... Next, we'll add (8) and (9) and integrate the sum throughout the volume of the cavity:

But  $\Delta\epsilon$  &  $\Delta\mu$  not assumed real!

$$\int_{V_c} \nabla \cdot (\bar{H} \times \bar{E}_0^* + \bar{H}_0^* \times \bar{E}) d\tau = \int_{V_c} [j\omega(\epsilon + \Delta\epsilon) \bar{E}_0^* \cdot \bar{E} - j\omega_0 \mu \bar{H} \cdot \bar{H}_0^* + j\omega(\mu + \Delta\mu) \bar{H}_0^* \cdot \bar{H} - j\omega_0 \epsilon \bar{E} \cdot \bar{E}_0^*] d\tau \quad (10)$$

Applying the divergence theorem to the LHS of (10) and combining terms on the RHS we find

$$\oint_S (\bar{H} \times \bar{E}_0^* + \bar{H}_0^* \times \bar{E}) \cdot \hat{n} ds = j \int_{V_c} \left\{ [\omega(\epsilon + \Delta\epsilon) - \omega_0 \epsilon] \bar{E} \cdot \bar{E}_0^* + [\omega(\mu + \Delta\mu) - \omega_0 \mu] \bar{H} \cdot \bar{H}_0^* \right\} d\tau \quad (11)$$

The integrand on the LHS of (11) is zero because

$$\begin{aligned} (\bar{H} \times \bar{E}_0^*) \cdot \hat{n} &= \bar{H} \cdot (\bar{E}_0^* \times \hat{n}) = 0 \quad \text{on pec} \\ (\bar{H}_0^* \times \bar{E}) \cdot \hat{n} &= \bar{H}_0^* \cdot (\bar{E} \times \hat{n}) = 0 \quad \text{on pec.} \end{aligned}$$

Consequently, (11) becomes

$$0 = \int_{V_c} \left\{ [\omega(\epsilon + \Delta\epsilon) - \omega_0 \epsilon] \bar{E} \cdot \bar{E}_0^* + [\omega(\mu + \Delta\mu) - \omega_0 \mu] \bar{H} \cdot \bar{H}_0^* \right\} d\tau \quad (12)$$

st.

$$\begin{aligned} 0 &= \int_{V_c} (\omega\epsilon - \omega_0\epsilon) \bar{E} \cdot \bar{E}_0^* d\tau + \int_{V_c} (\omega\mu - \omega_0\mu) \bar{H} \cdot \bar{H}_0^* d\tau \\ &+ \int_{V_c} \omega\Delta\epsilon \bar{E} \cdot \bar{E}_0^* d\tau + \int_{V_c} \omega\Delta\mu \bar{H} \cdot \bar{H}_0^* d\tau \end{aligned}$$

or

$$0 = (\omega - \omega_0) \int_{V_c} (\epsilon \bar{E} \cdot \bar{E}_0^* + \mu \bar{H} \cdot \bar{H}_0^*) dV$$

$$+ \omega \int_{V_c} (\Delta \epsilon \bar{E} \cdot \bar{E}_0^* + \Delta \mu \bar{H} \cdot \bar{H}_0^*) dV$$

Consequently, we find that

$$\frac{\omega - \omega_0}{\omega} = \frac{-\int_{V_c} (\Delta \epsilon \bar{E} \cdot \bar{E}_0^* + \Delta \mu \bar{H} \cdot \bar{H}_0^*) dV}{\int_{V_c} (\epsilon \bar{E} \cdot \bar{E}_0^* + \mu \bar{H} \cdot \bar{H}_0^*) dV} \quad (13)$$

This is an exact formula for the computation of the change in resonant frequency when a relative lossless cavity material is replaced with another (possibly lossy!) cavity material, assuming the walls are pec. (Note that  $\Delta \epsilon$  :  $\Delta \mu$  were not assumed or required to be real.)

...

### Perturbational Approximation

Equ. (13) is an exact expression but it is difficult to use since  $\bar{E}$  and  $\bar{H}$  are generally not known. These are the fields inside the cavity w/ the material introduced.

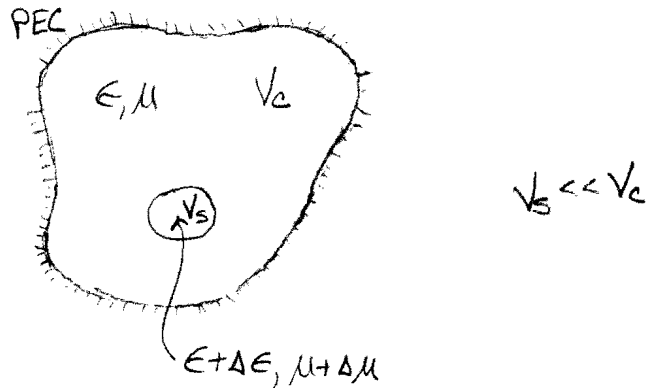
...even the case of a sample placed inside the cavity, (13) becomes

note!! why?

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$$\frac{\omega - \omega_0}{\omega} = \frac{-\int_{V_s} (\Delta\epsilon \bar{\mathbf{E}} \cdot \bar{\mathbf{E}}_0^* + \Delta\mu \bar{\mathbf{H}} \cdot \bar{\mathbf{H}}_0^*) dV}{\int_{V_c} (\epsilon \bar{\mathbf{E}} \cdot \bar{\mathbf{E}}_0^* + \mu \bar{\mathbf{H}} \cdot \bar{\mathbf{H}}_0^*) dV} \quad (14)$$

where  $V_s$  is the volume of the specimen.



We will assume the specimen size is very small w.r.t. wavelength, and that the specimen volume is small w.r.t.  $V_c$ . In the denominator of (14) we'll approximate

$$\int_{V_c} (\epsilon \bar{\mathbf{E}} \cdot \bar{\mathbf{E}}_0^* + \mu \bar{\mathbf{H}} \cdot \bar{\mathbf{H}}_0^*) dV \approx \int_{V_c} (\epsilon |\bar{\mathbf{E}}_0|^2 + \mu |\bar{\mathbf{H}}_0|^2) dV \quad (15)$$

This is reasonable because the contribution from  $V_s$  in the <sup>denominator of (14)</sup> is small w.r.t. the remainder of the cavity volume for a small specimen perturbation.

(Not assuming  $\Delta\epsilon$  and/or  $\Delta\mu$  are small.)

(Check stored energy expression. Power has  $\frac{1}{4}$  factor, rather than  $\frac{1}{2}$ .)

Notice that we're not <sup>necessarily</sup> assuming  $\vec{E} \approx \vec{E}_0$  and  $\vec{H} \approx \vec{H}_0$  within the specimen or in its vicinity. In fact, we haven't made any assumptions about  $\Delta\epsilon$  or  $\Delta\mu$ . These may even be large. Rather, (15) is reasonable in the context that the contribution to the integral from  $V_s$  is small w.r.t the remainder of the cavity volume.

Consequently, (14) becomes

Harrington,  
eqn (7-10):

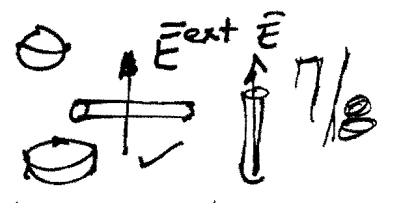
$$\frac{\omega - \omega_0}{\omega} \approx \frac{- \int_{V_s} (\Delta\epsilon \vec{E} \cdot \vec{E}_0^* + \Delta\mu \vec{H} \cdot \vec{H}_0^*) dV}{\int_{V_c} (\epsilon |\vec{E}_0|^2 + \mu |\vec{H}_0|^2) dV} \quad (16)$$

There are quite a few paths we can take from here using (16). This equation is a common starting point for many methods to extract  $\Delta\epsilon$  and/or  $\Delta\mu$  of specimens in a resonant cavity.

Let's consider a nonmagnetic specimen ( $\Delta\mu = 0$ ) or with a dielectric-magnetic specimen placed in a region of the cavity where  $\vec{H}_0 = 0$ , then (16) becomes

$$\begin{aligned} \frac{\omega - \omega_0}{\omega} &\approx \frac{- \int_{V_s} \Delta\epsilon \vec{E} \cdot \vec{E}_0^* dV}{\int_{V_c} \epsilon |\vec{E}_0|^2 dV} \\ &= - \frac{\Delta\epsilon}{\epsilon} \frac{\int_{V_s} \vec{E} \cdot \vec{E}_0^* dV}{\int_{V_c} |\vec{E}_0|^2 dV} \end{aligned} \quad (17)$$

...if we consider  $C_2 = \frac{\int_{V_s} \mathbf{E} \cdot \bar{\mathbf{E}}_0^* d\tau}{\int_{V_c} |\mathbf{E}_0|^2 d\tau}$  (18) to be a factor



...relatively insensitive to sample permittivity, then we  
...can use (17) to determine  $\Delta\epsilon$ .

...To accomplish this, we use a specimen of known permittivity  
...to calibrate by determining  $C_1$  from the change in resonant  
...frequency. Then specimens of similar shape and size  
...can be determined from a change in resonant frequency  
...using (17).

...Another situation is small  $\Delta\epsilon$  &  $\Delta\mu$ . In the limit as  
... $\Delta\epsilon \rightarrow 0$ ,  $\Delta\mu \rightarrow 0$ , there will only be a slight change to  $\bar{\mathbf{E}}$  and  $\bar{\mathbf{H}}$   
...from the unperturbed case. Hence, in (16) we can replace  
... $\bar{\mathbf{E}} \rightarrow \bar{\mathbf{E}}_0$  &  $\bar{\mathbf{H}} \rightarrow \bar{\mathbf{H}}_0$ , giving

Harrington  
eqn (7-11):

$$\frac{\omega - \omega_0}{\omega} \approx \frac{-\int_{V_s} (\Delta\epsilon |\bar{\mathbf{E}}_0|^2 + \Delta\mu |\bar{\mathbf{H}}_0|^2) d\tau}{\int_{V_c} (\epsilon |\bar{\mathbf{E}}_0|^2 + \mu |\bar{\mathbf{H}}_0|^2) d\tau} \quad (19)$$

...From this result, if  $\Delta\epsilon$  and/or  $\Delta\mu$  increase the resonant  
...frequency will decrease.

...In the case of a non-magnetic ( $\Delta\mu = 0$ ) or with the  
...specimen placed in a region of the cavity where  $\bar{\mathbf{H}}_0 \approx 0$ , then  
... (19) becomes

$$\frac{\omega - \omega_0}{\omega} \approx \frac{-\int_{V_s} \Delta \epsilon |\bar{E}_0|^2 dV}{\int_{V_c} \epsilon |\bar{E}_0|^2 dV} = -\frac{\Delta \epsilon}{\epsilon} C_2 \quad (20)$$

where

$$C_2 = \frac{-\int_{V_s} |\bar{E}_0|^2 dV}{\int_{V_c} \epsilon |\bar{E}_0|^2 dV} \quad (21)$$

Here,  $C_2$  is only a function of the cavity geometry and the position of the specimen. This can be determined by calibration with a known specimen, but here the specimen & the calibration specimen don't necessarily need to be the same shape. Changes in resonant frequency in (20) can be used to find  $\Delta \epsilon$ .

Add discussion on complex  $\omega$ . Use to determine  $\epsilon' & \epsilon''$  from  $\Delta \omega & \Delta Q$  measurements. Use lossless equations & complex  $\omega$ .  $\left[ \underset{\text{lossless resonator}}{\omega_0} \rightarrow \underset{\text{lossy resonator}}{\omega_0} \left(1 + \frac{j}{2Q_0}\right) \right]$   
 Reson. eqn (6.10)

Notice in (19) & (20) that  $\omega$  will be a complex number if specimen permittivity is complex ( $\Delta \epsilon = \text{complex}$ ). The complex angular frequency is related to the real resonant frequency of the cavity &  $Q$  of the cavity by

$$\omega = \omega_r + j\omega_i$$

$$\omega_r = 2\pi f_c$$

$$\therefore Q = \frac{\omega_r}{2\omega_i}$$