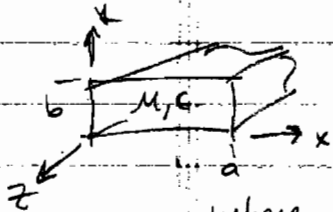


General Behavior  
of Rectangular Waveguides

The dispersion relation for a rectangular waveguide is very similar for  $TE^z$  &  $TM^z$  modes. We found in the last lecture, for wave prop in  $+z$ , that



$$\beta_{xm}^2 + \beta_{yn}^2 + \beta_{zmn}^2 = \beta^2 = \omega^2 \mu \epsilon \quad (1)$$

where  $\beta_{xm} = \frac{m\pi}{a}$   $m=0, 1, 2, \dots$   $\begin{cases} m=n \neq 0 & TE^z \\ m \neq 0 & TM^z \end{cases} \quad (2)$

$$\beta_{yn} = \frac{n\pi}{b} \quad n=0, 1, 2, \dots \quad (3)$$

and for  $TE^z$  modes  $m=n \neq 0$  while for  $TM^z$  modes  $m \neq 0$  &  $n \neq 0$ .

The form of the wave propagation in  $+z$  is  $e^{-j\beta_{zmn}z}$  and the longitudinal wave number is from (1).

$$\beta_{zmn} = \pm \sqrt{\beta^2 - \beta_{xm}^2 - \beta_{yn}^2} \quad (4)$$

There are an infinite # of these modes  $mn$  that are generally "excited" when a source is applied to the waveguide. Each of these modes is identified by it's indices  $m$  &  $n$  as  $TE_{mn}^z$  &  $TM_{mn}^z$ . How "much" of each mode contributes to the total field depends on the specific excitation.



We will study the general solutions to the waveguide (the eigen spectrum) & not concern ourselves w/ the general excitation. Very difficult analysis.  
(See R.E. Collin, "Field Theory of Guided Waves.")

These modes in the waveguide have a very unusual characteristic we can see from (4). We'll define

$$\beta_{cmn}^2 = \beta_{xm}^2 + \beta_{yn}^2 \quad (5)$$

so that (4) reads

$$\beta_{zmn} = \pm \sqrt{\beta^2 - \beta_{cmn}^2} \quad (6)$$

Notice in (6) that when  $\beta^2 < \beta_{cmn}^2$  the wave is purely attenuated while when  $\beta^2 > \beta_{cmn}^2$  the wave is purely propagating.  $\beta^2$  is a function of frequency ( $\neq \mu \neq \epsilon$ ) while  $\beta_{cmn}^2$  is dependent on dimensions  $a, b$  as well as indices  $m, n$ .

When  $\beta^2 = \beta_{cmn}^2$  the wave is neither propagating nor attenuating. It is called cut off. For this reason,  $\beta_{cmn}$  is called the cutoff wavenumber.

$$\text{Hence, from (5)} \quad \beta_{cmn} = \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2} \quad (7)$$

$$\text{Also, from (6)} \quad \beta_{cmn} = \beta \Big|_{\beta_{zmn}=0} = \omega_{cmn} \sqrt{\mu\epsilon} = 2\pi f_{cmn} \sqrt{\mu\epsilon} \quad (8)$$

where  $f_{cmn}$  is the cutoff frequency of mode  $mn$ .

Using (8) in (7),  $f_{c_{mn}} = \frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$  (3.84)(9)

Let's take an X-band rectangular waveguide as an example. This is called a WR-90 waveguide.

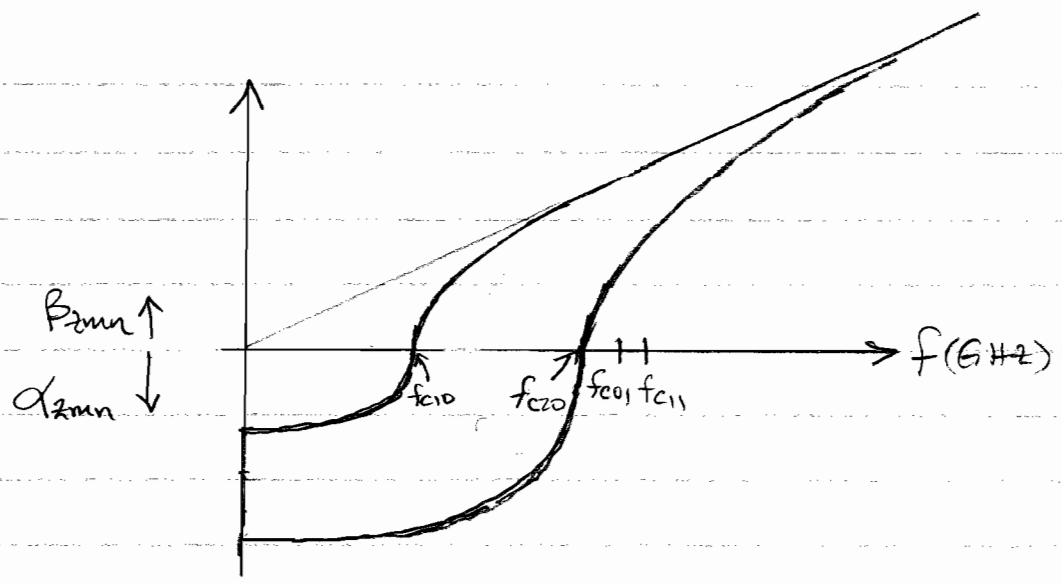
From Appendix I,

Inside dimensions  $a = 0.90''$  (2.286 cm) ;  $b = 0.40''$  (1.016 cm). <sup>Assuming air-filled,</sup> The first 10 modes with the lowest cutoff frequencies are

- |     |                  |                        |                    |
|-----|------------------|------------------------|--------------------|
| 1.  | TE <sub>10</sub> | $f_{c10} = 6.562$ GHz  |                    |
| 2.  | TE <sub>20</sub> | $f_{c20} = 13.124$ GHz |                    |
| 3.  | TE <sub>01</sub> | $f_{c01} = 14.764$ GHz |                    |
| 4.  | TE <sub>11</sub> | $f_{c11} = 16.56$ GHz  | } degenerate modes |
| 5.  | TM <sub>11</sub> | "                      |                    |
| 6.  | TE <sub>30</sub> | $f_{c30} = 19.685$ GHz |                    |
| 7.  | TE <sub>21</sub> | $f_{c21} = 19.754$ GHz | } degenerate       |
| 8.  | TM <sub>21</sub> | "                      |                    |
| 9.  | TE <sub>31</sub> | $f_{c31} = 24.607$ GHz | } degenerate       |
| 10. | TM <sub>31</sub> | "                      |                    |

The mode with the smallest  $f_c$  is called the dominant mode. For this waveguide having  $a > b$ , the dominant mode is TE<sub>10</sub>.

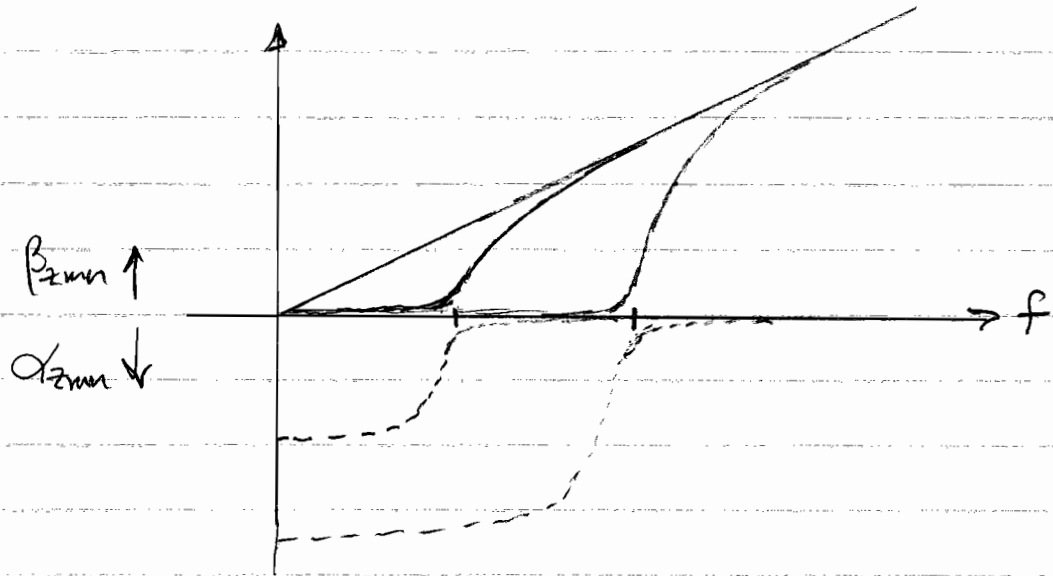
Let's plot  $\beta_{z10}$



For  $f < f_{c10}$ , no modes prop. They are purely attenuated. (Fields near source are not zero, however, they are reactive <sup>type of this mode</sup> fields yielding reactive input impedance)

For  $f_{c10} < f < f_{c20}$  only one mode will propagate. All others purely attenuated. Most often will operate WVDs in single mode. For this particular WVD, single mode operation is possible <sup>ideally</sup> from 6.562 GHz to 13.124 GHz.

This is assuming no loss. Metal losses <sup>if small</sup> tend to "smear out" the response such as



There is another characteristic of wave propagation in hollow metallic waveguides that is very apparent from these plots of  $\beta_{zmn}$ . These waveguides are dispersive, even when there are no losses! (Metallic losses would add further dispersion.)

That is,  $\omega e^{-j\beta_{zmn}z}$  propagation, the phase velocity is dependent on frequency. By definition, the phase velocity  $v_p$  is given as

$$v_p = \frac{\omega}{\beta}$$

For prop in  $+z$ , the phase velocity  $v_p$  in that direction is

$$v_{pz} = \frac{\omega}{\beta_{zmn}} = \frac{\omega}{\sqrt{\beta^2 - \beta_{cnn}^2}} \quad \beta^2 > \beta_{cnn}^2 \quad (9)$$

Unlike plane waves in lossless media,  $v_{pz}$  is a fct. of frequency.

Similarly, the group velocity  <sup>$v_p$</sup>  is also a function of  $f$ . This velocity is defined as the inverse slope of the dispersion curve ( $\beta_z - \omega$ ):

$$v_{gz} = \frac{\partial \omega}{\partial \beta_{zmin}}$$

Group velocity  $\rightarrow$  speed of information transmission (energy)

Instruction to plot the phase & group velocities:

