

## Section 13.2

Equivalent circuit model for mutually coupled inductors

Now that we've discussed the electrical behavior of coupled inductors, we'll now move to the analysis of circuits containing such elements. To that end, consider the circuit of Fig. 13.7(a).

Fig. 13.7(a)

Applying KVL to coil 1 
$$V_1 = i_1 R_1 + L_1 \frac{di_1}{dt} + \underbrace{M \frac{di_2}{dt}}_{(13.16)} \quad (13.20a)$$

and KVL to coil 2: 
$$V_2 = i_2 R_2 + L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \quad (13.20b)$$

Much of our circuit analysis will be for sinusoidal steady state, so in the frequency domain, these two eqns read

$$V_1 = R_1 \bar{I}_1 + j\omega L_1 \bar{I}_1 + j\omega M \bar{I}_2 \quad (13.21a)$$

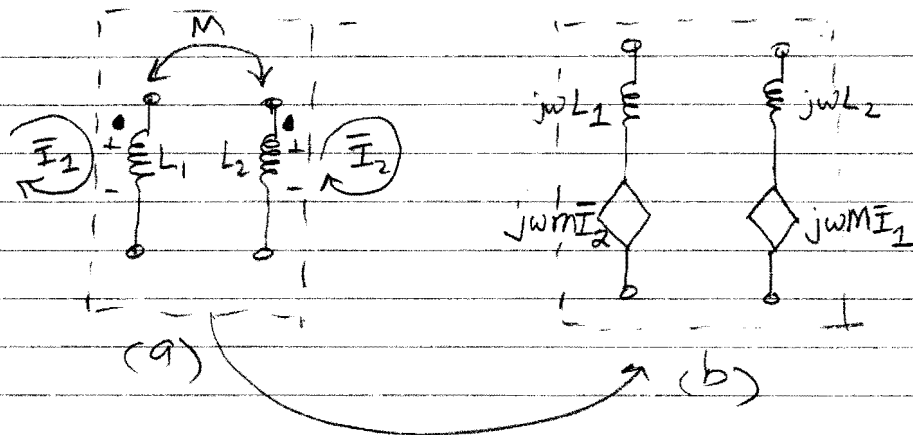
$$V_2 = R_2 \bar{I}_2 + j\omega L_2 \bar{I}_2 + j\omega M \bar{I}_1 \quad (13.21b)$$

The second term in each eqn. is the <sup>voltage produced by the</sup> ~~impedance~~ of the inductor itself while the third represents a voltage produced by the current in the other coil.

We could analyze such a system of equations in (13.21) in a brute force manner. There are two linearly independent equations. Provided we are supplied with sufficient information (enough  $V$ 's &  $I$ 's) we could solve for up to two unknowns.

But things are tricky with ccts. containing coupled inductors. Including the  $M \frac{di}{dt}$  term isn't obvious, and the dot convention business can easily lead to important sign errors.

To aid us in properly incorporating both of these concepts, there is a very, very useful equivalent circuit for coupled inductors shown in Fig. 13.8:



In this equivalent circuit model for coupled inductors, the  $M$  symbol has been replaced with something far more valuable and helpful: 2 dependent voltage sources. These come from eqns (13.21a) & (13.21b) the last terms in

→ So as a first step in ckt analysis, we replace the coupled L's with equiv. ckt of Fig. 13.8b) But notice the polarity of the dependent voltage sources are not yet shown. This is where the dot convention comes into play.

Remember from Fig. 13.5(a), in frequency domain

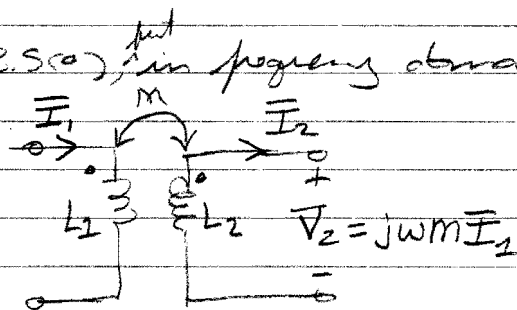
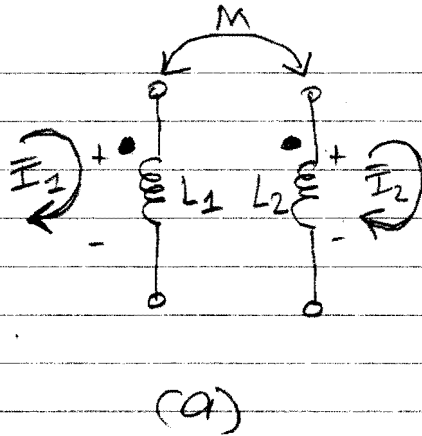


Fig. 1

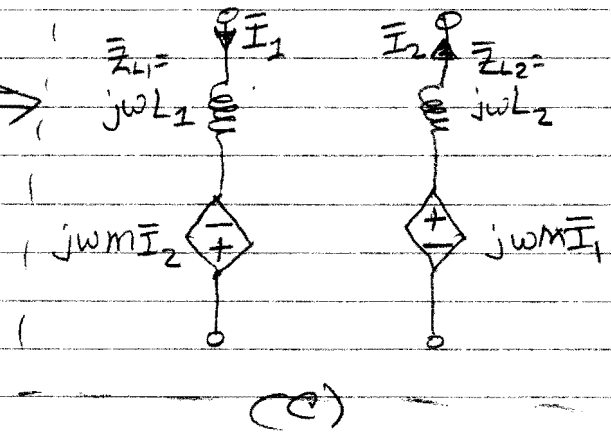
With  $I_1$  into dotted terminal,  $V_2$  positive with polarity of  $V_2$  as shown. That is, w/ '+' at dotted terminal for  $V_2$ .

In such a circuit, the current  $I_1$  induces a voltage  $V_2$  in "port" 2. This induced voltage  $V_2$  acts as a source trying to "push" or "expel" charges from port 2, with  $I_2$  positive as shown in the fig above, Fig. 1.

Knowing this behavior allows us to properly assign the signs of the dependent voltage sources in Fig. 13.8b). Because  $I_1$  enters the dotted terminal in Fig. 1, the effects of mutual inductance will work to expel charges from the dotted terminal in port 2. induce a voltage in coil 2 that tries to



Eqn.  $\xrightarrow{\text{ckt.}}$

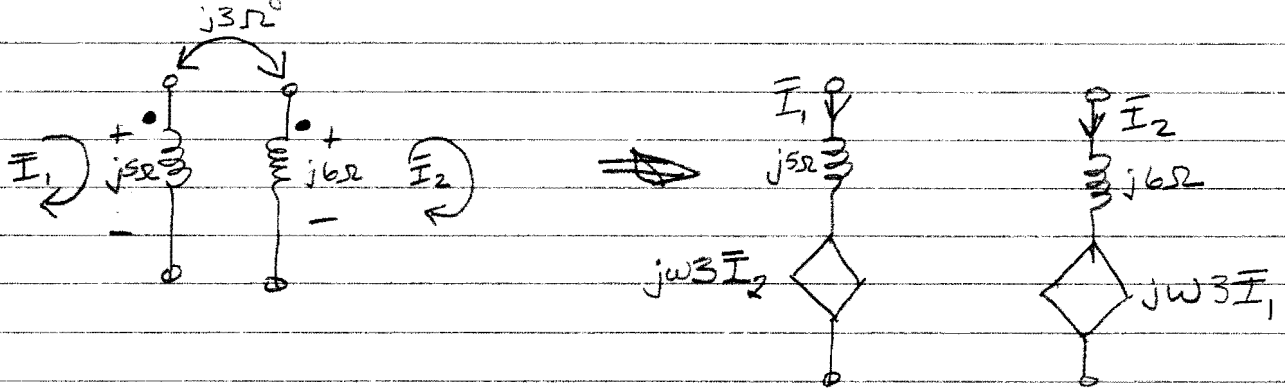


Now we simply insert this equivalent circuit into the original circuit in place of the original mutual inductance and solve the circuit in a straight forward manner as we would in Circuits I.

The effects of mutual inductance and the complexities and pitfalls of the dot convention have all been incorporated into the equivalent circuit of Fig. 13.8(c).

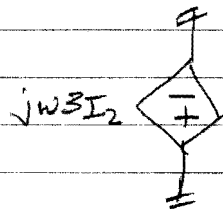
Example 13.1. Calculate the currents  $\bar{I}_1$  &  $\bar{I}_2$  in the circuit of Fig. 13.9(a).

The first step is to replace the mutual inductance with its equivalent circuit model of Fig. 13.8(b) - w/o the signs in the dependant voltage sources

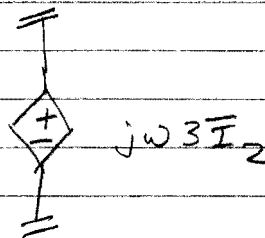


Then add the signs to the dependant voltage sources:

- $\bar{I}_2$  into non-dotted terminal induces '-' voltage in part 1  
 $\Rightarrow$  pushing current out of non-dotted terminal:



- $\bar{I}_1$  into dotted terminal induces '+' voltage in part 2  
 $\Rightarrow$  pushing current out of dotted terminal:



This gives the equivalent circuit of Fig. 13.9(b)

Fig 13.9(b)

The remaining part of the problem is to simply solve for  $\bar{I}_1$  &  $\bar{I}_2$  in Fig. 13.9(b) using circuit analysis skills from Circuits I.

$$\text{KVL in Loop 1: } 12 = (-j4 + j5)\bar{I}_1 - j3\bar{I}_2$$

$$\text{or } j\bar{I}_1 - j3\bar{I}_2 = 12 \quad (13.1.1)$$

$$\text{KVL in Loop 2: } j3\bar{I}_1 = j6\bar{I}_2 + 12\bar{I}_2 = (12 + j6)\bar{I}_2$$

$$\Rightarrow \bar{I}_1 = \frac{12 + j6}{j3}\bar{I}_2 = (2 - j4)\bar{I}_2 \quad (13.1.2)$$

$$\text{Sub this into 13.1.1: } j(2 - j4)\bar{I}_2 - j3\bar{I}_2 = 12$$

$$\text{or } j2 + 4\bar{I}_2 - j3\bar{I}_2 = (4 - j1)\bar{I}_2 = 12$$

$$\therefore \bar{I}_2 = \underline{2.91 \angle 14.04^\circ \text{ A}} \quad (13.1.3)$$

$$\bar{I}_1 = (2 - j4)\bar{I}_2 = \underline{13.01 \angle -49.39^\circ \text{ A}}$$

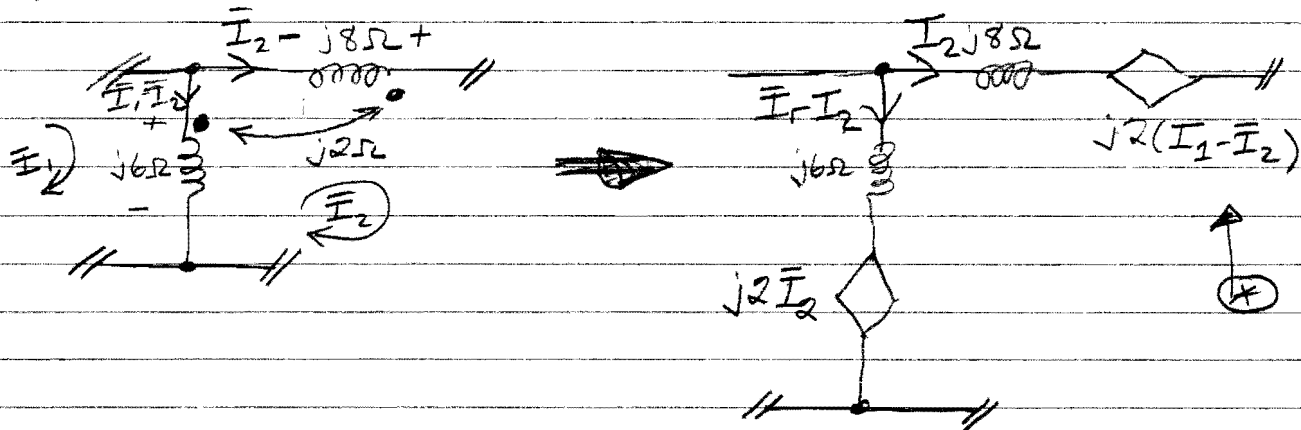
↑  
(13.1.2)

mesh

Example 13.2 Calculate the  $\vec{I}_1, \vec{I}_2$  in the ckt. of Fig. 13.11.

Fig. 13.11

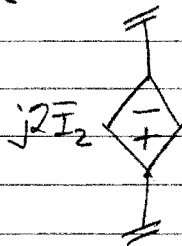
To begin, we replace the mutual inductance with the equivalent circuit model:



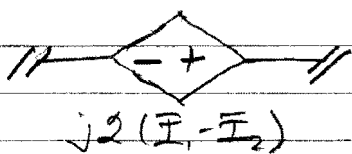
Notice the  $\vec{I}_1 - \vec{I}_2$  current: we're solving for mesh currents, not branch currents, so the current in the  $j6\Omega$  inductor is  $\vec{I}_1 - \vec{I}_2$ .

For the polarity of the dependent voltage sources:

- $\vec{I}_2$  into non-dotted terminal of  $j8$  induces negative voltage in  $j6$ , which creates tendency to push charges out of non-dotted terminal.



- $\vec{I}_1 - \vec{I}_2$  into dotted terminal of  $j6$  induces positive voltage w/ polarity indicated across  $j8$ . This creates propensity to push charges out of the dotted terminal of  $j8$ .



Applying KVL to loop 1 in Fig 13.11 using equivalent circuit of Fig 13.12

$$100 \angle 0^\circ = (4 - j3) \bar{I}_1 + j6(\bar{I}_1 - \bar{I}_2) - j2 \bar{I}_2$$

$$\text{or } 100 = (4 + j3) \bar{I}_1 - j8 \bar{I}_2 \quad (13.2.2)$$

Then applying KVL to loop 2,

$$j2 \bar{I}_2 + j6(\bar{I}_2 - \bar{I}_1) + j8 \bar{I}_2 - j2(\bar{I}_1 - \bar{I}_2) + 5 \bar{I}_2 = 0$$

$$\text{or } \bar{I}_1(-j6 - j2) + \bar{I}_2(j2 + j6 + j8 + j2 + 5) = 0$$

$$\text{or } 0 = -j8 \bar{I}_1 + (5 + j18) \bar{I}_2 = 0 \quad (13.2.2)$$

$$\Rightarrow \bar{I}_1 = \frac{5 + j18}{j8} \bar{I}_2 = (2.250 - j0.625) \bar{I}_2 \quad (1)$$

Sub this into (13.2.2) gives

$$100 = (4 + j3) \cdot (2.250 - j0.625) \bar{I}_2 - j8 \bar{I}_2$$

$$= (10.875 + j4.25) \bar{I}_2 - j8 \bar{I}_2 = (10.875 - j3.75) \bar{I}_2$$

$$\therefore \underline{\bar{I}_2} = 8.218 + j2.834 = \underline{8.693 \angle 19.03^\circ} \text{ A} \quad (2)$$

and sub (2)  $\rightarrow$  (1)

$$\underline{\bar{I}_1} = (2.250 - j0.625) \cdot (8.218 + j2.834) = 20.262 + j1.240$$

$$= \underline{20.300 \angle 3.50^\circ} \text{ A}$$